



## Interface study of carbon fibre reinforced Al–Cu composites

Z.G. Liu<sup>a,b,c,\*</sup>, X.B. Mang<sup>c</sup>, L.H. Chai<sup>c</sup>, Y.Y. Chen<sup>c</sup>

<sup>a</sup> Key Laboratory of Micro-systems and Micro-structures Manufacturing (Harbin Institute of Technology), Ministry of Education, Harbin 150001, China

<sup>b</sup> State Key Laboratory of Advanced Welding Production Technology, Harbin 150001, China

<sup>c</sup> School of Materials Science and Engineering, Harbin Institute of Technology, Harbin 150001, China

### ARTICLE INFO

#### Article history:

Received 5 July 2009

Received in revised form 13 April 2010

Accepted 16 April 2010

Available online 22 April 2010

#### Keywords:

Composite

Carbon fibre

Microstructure

Interface

### ABSTRACT

The application of continuous carbon fibre-reinforced aluminium matrix composites ( $C_f/Al$ ) in aerospace, automobile, and electric power cable industries is of considerable interest because of their high specific strength, specific modulus, and low coefficient of thermal expansion. In this paper, we report the study on the alloy contribution to the interface of a carbon fibre reinforced aluminium alloy matrix composite. The composites were produced using squeeze casting technology. An Al–Cu alloy was used as the matrix material. Detailed investigations revealed that the aluminium alloy melt fill in the gaps between fibres. The important feature is that the solidification microstructure of Al–Cu matrix alloy is altered by the presence of carbon fibre. The surface of carbon fibre acts as the nucleation site of  $Al_2Cu$  phase.  $Al_2Cu$  phase prefers to form at the interface between carbon fibre and Al–Cu alloys. Ni coated on carbon fibre does not change the feature.

© 2010 Elsevier B.V. All rights reserved.

### 1. Introduction

Carbon fibre ( $C_f$ ) reinforced aluminium matrix composites are of great interest because of their high specific strength and stiffness, low coefficient of thermal expansion, and high thermal/electrical conductivity [1]. These advantages make them potential structural and functional materials in such as automotive and aeronautic applications [2]. Some different techniques have been developed to fabricate such composite materials, such as squeeze casting, metal spray and metal infiltration [3].

However, the poor wetting characteristics of carbon by liquid aluminium and reaction of carbon fibres with some aluminium alloys hindered the development of  $Al/C_f$  composites [4]. Improper wetting and chemical reactions at the interface during synthesis or under service conditions can degrade the mechanical properties of the composites. The reaction at the carbon–aluminium interface when produced in liquid state was also considered to affect critically the strength of  $Al/C_f$  composites [5] by influence the load transfer from fibre to matrix. Formation of  $Al_4C_3$  may deteriorate the strength of carbon fibre. However, the liquid processes have several advantages on other production routes, such as high production rate, low cost and potential of production of complex parts are some of them.

Though many investigations [6–10] have been concentrated on fabrication, tensile properties and fracture behavior of Al reinforced with continuous carbon fibre, not too much attention has been paid on the influence of alloy matrix. Therefore, in this investigation, an attempt has been made to elucidate the influence of the alloy on the microstructure of aluminium matrix composites produced by squeeze casting method.

### 2. Experimental

The matrix aluminium alloy used in the present study is an Al–Cu alloy. Table 1 presents the chemical composition of the alloy. Carbon fibre used in the present study is T-300, with a diameter of  $7\ \mu\text{m}$  (Fig. 1a). The volume fraction of carbon fibre is 40%. Squeeze casting was performed on a YA32-200A hydraulic presser with a maximum pressure of 2000 kN. The parameters of squeeze casting were as follows: Al–Cu melt casting temperature is  $730\ ^\circ\text{C}$ ; preheat the casting mould to  $550\ ^\circ\text{C}$  before casting; squeeze pressure is 100 MPa; pressure holding time is 2 min. Surface treatment of carbon fibre by Ni electroplating (Fig. 1b) was performed to study the contribution of surface treatment of carbon fibre during squeeze casting.

The microstructure characterization of produced specimens was performed on a Hitachi S-4700 scanning electron microscope. The phase determination was carried out on a Rigaku D-max-rB X-ray diffractometer (XRD) with a Cu target ( $\lambda = 0.15418\ \text{nm}$ ).

### 3. Results and discussions

Fig. 2 shows the microstructure of matrix Al–Cu alloy. Al grains are very coarse (roughly  $100\text{--}300\ \mu\text{m}$ ) with some eutectic structure (bright phase). EDS analysis revealed that the bright grey phase is  $Al_2Cu$  phase (Al:Cu = 67.3:32.7). XRD analysis confirmed that the alloy is composed of Al phase and  $Al_2Cu$  phase (Fig. 3).

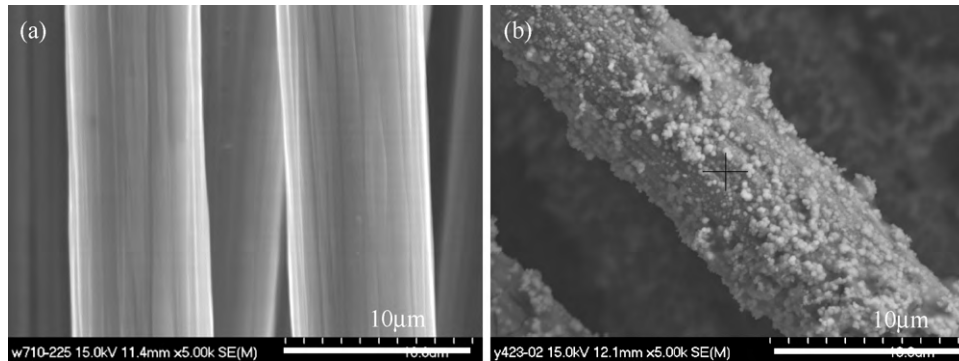
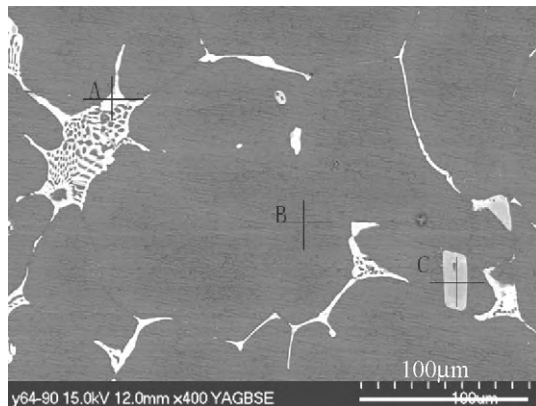
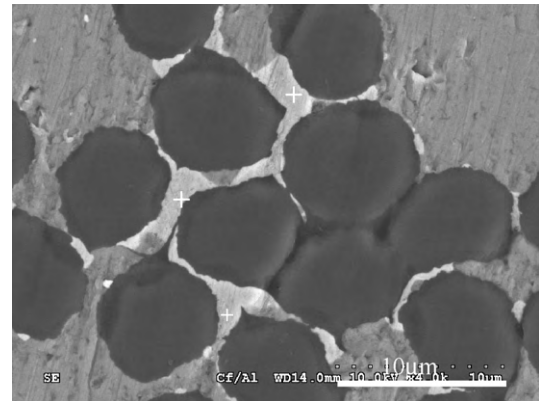
\* Corresponding author at: Key Laboratory of Micro-systems and Micro-structures Manufacturing (Harbin Institute of Technology), Ministry of Education, Harbin 150001, China. Tel.: +86 451 86418802; fax: +86 451 86418802.

E-mail address: [zhiguang@hit.edu.cn](mailto:zhiguang@hit.edu.cn) (Z.G. Liu).

**Table 1**

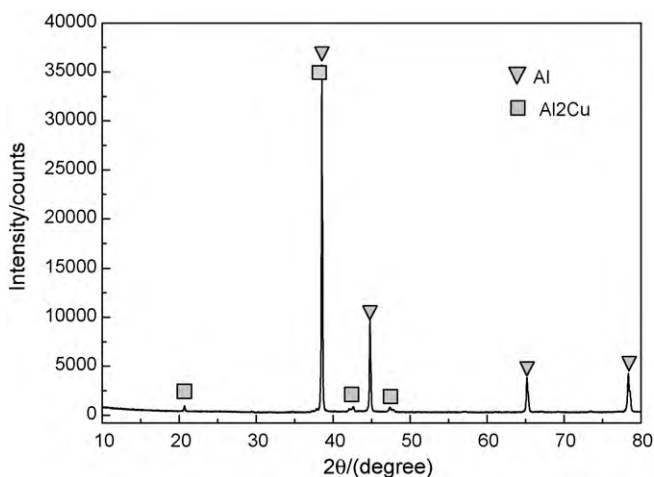
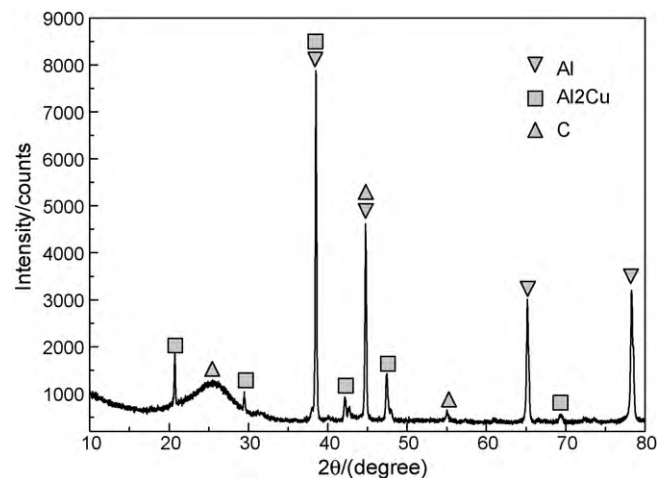
Chemical composition of Al alloy used as matrix.

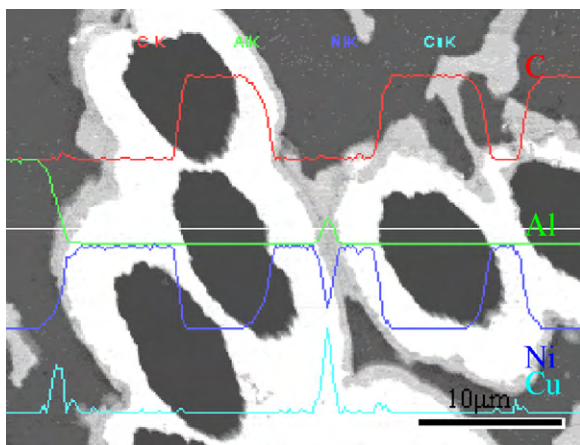
| Element              | Cu      | Mn      | Ti        | Ca        | Zr        | V        | B          | Al      |
|----------------------|---------|---------|-----------|-----------|-----------|----------|------------|---------|
| Concentration (wt.%) | 4.6–5.3 | 0.3–0.5 | 0.15–0.35 | 0.15–0.25 | 0.05–0.20 | 0.05–0.3 | 0.005–0.06 | Balance |

**Fig. 1.** SEM images of carbon fibre used in the present study: (a) without and (b) with Ni coating.**Fig. 2.** BSE image showing microstructure of Al–Cu matrix alloy. Al matrix (B) and eutectic structure can be identified (A region). Region C is Al enriched with Ti and V.**Fig. 4.** SEM image showing microstructure of  $C_f/Al$  composite with carbon fibre not coated with Ni.  $Al_2Cu$  phase around carbon fibre is clearly shown (the bright region as cross indicated).

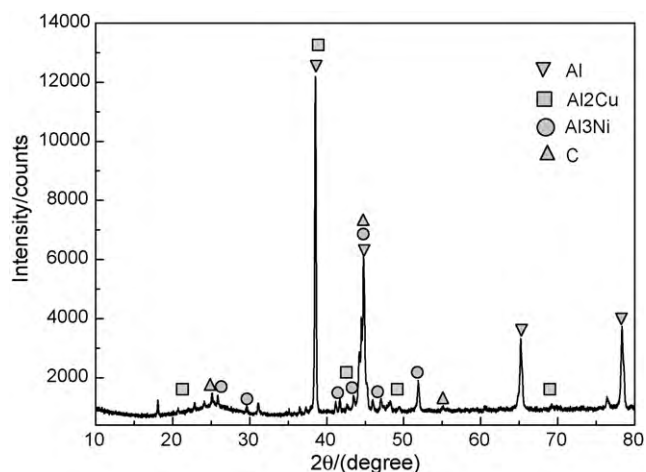
**Fig. 4** shows the microstructure of squeeze cast  $C_f/Al$  composite. It was found that Al matrix appears grey while carbon fibre appears dark. Between carbon fibre and Al matrix there exist bright grey phase which was characterized as  $Al_2Cu$  phase by EDS analysis. XRD analysis also confirmed the existence of  $Al_2Cu$  phase (see **Fig. 5**). The diffused peak around  $26^\circ$  is determined as carbon. It has been

studied previously that during the solidification of this Al–Cu alloy, Al phase solidifies at higher temperature and the low melting point eutectic forms between the Al grains at lower temperature [11,12]. It seems that the  $Al_2Cu$  phase prefers to form around carbon fibre,

**Fig. 3.** XRD pattern of Al–Cu matrix alloy. Al and  $Al_2Cu$  phases were determined.**Fig. 5.** XRD pattern of  $C_f/Al$  composite with carbon fibre without Ni coating. Carbon, Al and  $Al_2Cu$  phases were determined.



**Fig. 6.** EDS line scanning (white horizontal line) showing the microstructure of  $C_f/Al$  composite with carbon fibre coated with Ni. Ni (white region) around carbon fibre (black oval) and  $Al_2Cu$  phase (bright grey region surrounding Ni region) around Ni are clearly shown.



**Fig. 7.** XRD pattern of  $C_f/Al$  composite with carbon fibre with Ni coating. Carbon, Al,  $Al_2Cu$  and  $NiAl_3$  phases were determined.

and therefore, the eutectic structure was reduced and eliminated around carbon fibre. No  $Al_4C_3$  phase was detected in this sample.

Fig. 6 shows the microstructure of squeeze cast  $C_f/Al$  composite with carbon fibre electroplated with Ni. It was interesting to notice that  $C_f/Al$  composite with carbon fibre electroplated with Ni shows similar microstructure to that with carbon fibre without Ni coat-

ing.  $Al_2Cu$  phase tends to form around carbon fibre preferentially. EDS line scanning revealed the existence of Ni coating and  $Al_2Cu$  phase. The eutectic structure was reduced and even eliminated as well around carbon fibre. However, one evidently different phenomenon is the formation of  $NiAl_3$  phase (see XRD patterns shown in Fig. 7). It is apparently from the reaction between electroplated Ni and Al melt during solidification. The formation of  $Al_4C_3$  phase was not observed. The reaction between carbon fibre and Al melt was hindered.

From the results above presented, it is found evidently that for Al–Cu alloy the introduction of carbon fibre significantly change the microstructure of matrix alloy. The eutectic structure was reduced and even eliminated around carbon fibre.  $Al_2Cu$  phase tends to form around carbon fibre no matter the carbon fibre is coated by Ni or not. It is suggested that carbon fibre supplies the nucleation of  $Al_2C$  phase during solidification process. Similar behaviour has been found in other carbon fibre reinforced Al alloys [12,13]. It is therefore believed that the control of matrix alloy composition and microstructure is also critical to the microstructure and properties of the composite.

#### 4. Conclusions

Investigation on the squeeze cast  $C_f/Al$ –Cu composite revealed that carbon fibre supplied preferential nucleation sites for  $Al_2Cu$  phase to form around carbon fibre during solidification. The characteristic eutectic structure of Al–Cu matrix alloy was reduced and eliminated. The surface treatment with electroplated Ni of carbon fibre does not change this feature at all. But the existence of Ni coating leads to the formation of  $NiAl_3$  phase by the reaction of Ni with Al melt.

#### References

- [1] E. Fitzer, L.M. Manoch, Carbon Reinforcements and Carbon–Carbon Composite, Springer, 1998.
- [2] O. Perez, G. Patriarche, M. Lancin, J. Phys. 3 (1993) 1693–1700.
- [3] K. Kuniya, H. Arakava, Carbon Fibre Reinforced Aluminum Composite Material, U.S. Patent No. 3,871,834 (1995).
- [4] S.H. Li, C. Chao, Metall. Mater. Trans. 35A (2004) 2153–2159.
- [5] J. Farahmandi, M. Dispennette, Aluminum–Carbon Composite Electrode, U.S. Patent No. 5,777,428 (1998).
- [6] T. Ohkawa, L. Jolla, H. Elsner, Fabrication of Fibre Reinforced Composites, U.S. Patent No. 5,468,358 (1995).
- [7] M.H. Vidal-Setif, M. Lancin, C. Marhic, R. Valle, J.L. Raviart, J.C. Daux, M. Rabinovitch, Mater. Sci. Eng. A272 (1999) 321–333.
- [8] J.F. Silvain, A. Proult, M. Lahaye, J. Douin, Compos.: Part A 34 (2004) 1143–1149.
- [9] A. Urena, J. Rams, M.D. Escalera, M. Sanchez, Compos. Sci. Technol. 65 (2005) 2025–2038.
- [10] G. Hackl, H. Gerhard, N. Popovska, Thin Solid Films 513 (2006) 217–222.
- [11] S.J. Chu, Y.F. Liu, H.W. Wang, Acta Compos. 14 (1997) 25–31.
- [12] P. He, Y.Z. Liu, D. Liu, Mater. Sci. Eng. A422 (2006) 333–338.
- [13] H.G. Seong, H.F. Lopez, D.P. Robertson, Mater. Sci. Eng. A 487 (2008) 201–209.